

The EN2390QI is a Power System on a Chip (PowerSoC) DC-DC converter. It integrates MOSFET switches, small-signal control circuits, compensation and an integrated inductor in an advanced 11x10x3mm QFN module. It offers high efficiency, excellent line and load regulation over temperature. The EN2390QI operates over a wide input voltage range and is specifically designed to meet the precise voltage and fast transient requirements of high-performance products. The EN2390QI features frequency synchronization to an external clock, power OK output voltage monitor, programmable soft-start along with thermal and short circuit protection. The device's advanced circuit design, ultra high switching frequency and proprietary integrated inductor technology delivers high-quality, ultra compact, non-isolated DC-DC conversion.

All Altera Enpirion products are RoHS compliant, halogen free and are compatible with lead-free manufacturing environments.

- Integrated Inductor, MOSFETS, Controller
- Total Solution Size Estimate: 235mm²
- Wide Input Voltage Range: 4.5V – 14V
- 1% Initial Output Voltage Accuracy
- Master/Slave Configuration for Parallel Operation
 - Up to 4 Devices with 29A capability
- Frequency Synchronization (External Clock)
- Output Enable Pin and Power OK Signal
- Programmable Soft-Start Time
- Under Voltage Lockout Protection (UVLO)
- Short Circuit Protection
- Thermal Shutdown Protection
- RoHS Compliant, MSL Level 3, 260°C Reflow

- Space Constrained Applications
- Distributed Power Architectures
- Output Voltage Ripple Sensitive Applications
- Beat Frequency Sensitive Applications
- Servers, Embedded Computing Systems, LAN/SAN Adapter Cards, RAID Storage Systems, Industrial Automation, Test and Measurement, and Telecommunications

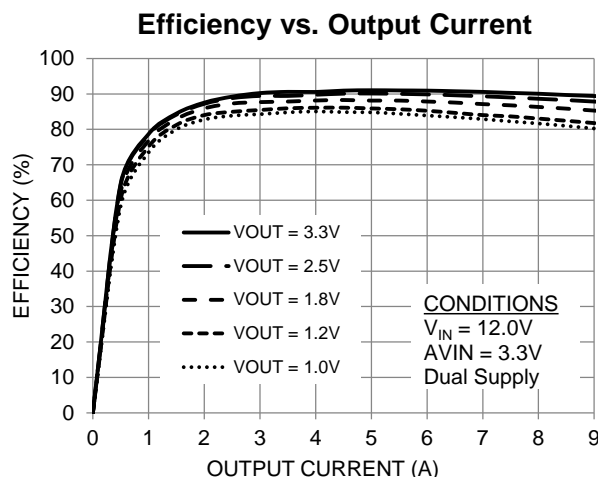


Figure 2. Highest Efficiency in Smallest Solution Size

Ordering Information

| Part Number | Package Markings | T _{AMBIENT} Rating (°C) | Package Description |
|--------------|------------------|----------------------------------|------------------------------------|
| EN2390QI | EN2390QI | -40 to +85 | 76-pin (11mm x 10mm x 3mm) QFN T&R |
| EVB-EN2390QI | EN2390QI | | QFN Evaluation Board |

Packing and Marking Information: www.altera.com/support/reliability/packing/rel-packing-and-marking.html

Pin Assignments (Top View)

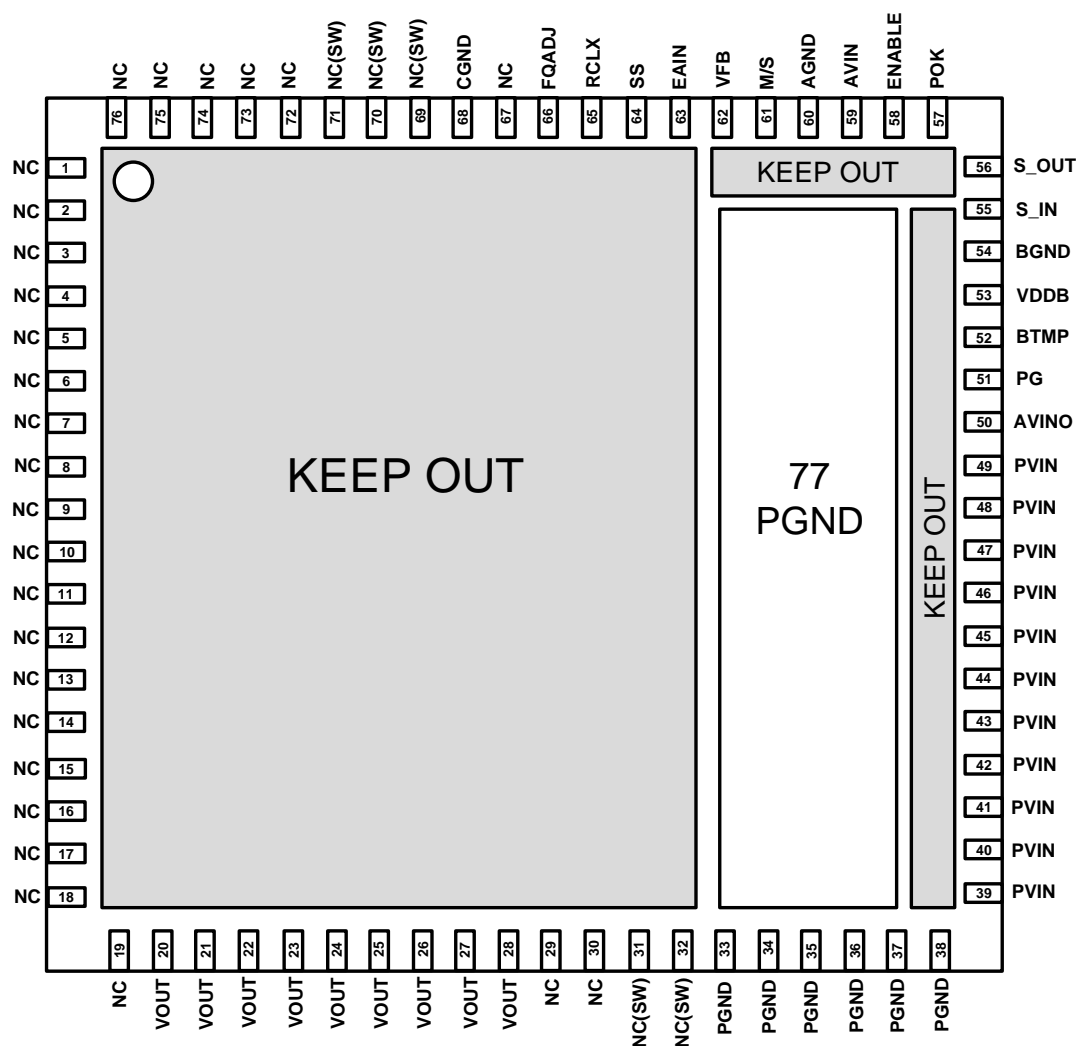


Figure 3: Pin Out Diagram (Top View)

NOTE A: NC pins are not to be electrically connected to each other or to any external signal, ground, or voltage. All pins including NC pins must be soldered to the PCB. Failure to follow this guideline may result in part malfunction or damage.

NOTE B: Shaded area highlights exposed metal below the package that is not to be mechanically or electrically connected to the PCB. Refer to Figure 16 for details.

NOTE C: White 'dot' on top left is pin 1 indicator on top of the device package.

Pin Description

I/O Legend: P=Power G=Ground NC=No Connect I=Input O=Output I/O=Input/Output

| PIN | NAME | I/O | FUNCTION |
|-------------------------|--------|-----|---|
| 1-19, 29, 30, 67, 72-76 | NC | NC | NO CONNECT – These pins may be internally connected. Do not connect them to each other or to any other electrical signal. Failure to follow this guideline may result in device damage. |
| 20-28 | VOUT | O | Regulated converter output. Connect these pins to the load and place output capacitor between these pins and PGND pins 33-35. |
| 31, 32, 69-71 | NC(SW) | NC | NO CONNECT – These pins are internally connected to the common switching node of the internal MOSFETs. They are not to be electrically connected to any external signal, ground, or voltage. Failure to follow this guideline may result in damage to the device. |
| 33-38 | PGND | G | Input/Output power ground. Connect these pins to the ground electrode of the input and output filter capacitors. See VOUT and PVIN pin descriptions for more details. |
| 39-49 | PVIN | P | Input power supply. Connect to input power supply. Decouple with input capacitor to PGND pins 36-38. |
| 50 | AVINO | O | Internal 3.4V linear regulator output. Connect this pin to AVIN for applications where operation from a single input voltage (PVIN) is required. If AVINO is being used, place a 1 μ F, X5R, capacitor between AVINO and AGND as close as possible to AVINO. |
| 51 | PG | I/O | PMOS gate. Place a 47nF, X5R, capacitor between this pin and BTMP. |
| 52 | BTMP | I/O | Bottom plate ground. See pin 51 description. |
| 53 | VDDDB | O | Internal regulated voltage used for the internal control circuitry. Place a 0.22 μ F, X5R, capacitor between this pin and BGND. |
| 54 | BGND | G | Ground for VDDDB. Do not connect BGND to any other ground. See pin 53 description. |
| 55 | S_IN | I | Digital synchronization input. This pin accepts either an input clock to phase lock the internal switching frequency or a S_OUT signal from another EN2390QI. Leave this pin floating if not used. |
| 56 | S_OUT | O | Digital synchronization output. PWM signal is output on this pin. Leave this pin floating if not used. |
| 57 | POK | O | Power OK is an open drain transistor (pulled up to AVIN or similar voltage) used for power system state indication. POK is logic high when VOUT is within -10% to +20% of VOUT nominal. Leave this pin floating if not used. |
| 58 | ENABLE | I | Output enable. Applying a logic high to this pin enables the output and initiates a soft-start. Applying a logic low disables the output. ENABLE logic cannot be higher than AVIN (refer to Absolute Maximum Ratings). Do not leave floating. See Power Up/Down Sequencing section for details. |
| 59 | AVIN | P | 3.3V Input power supply for the controller. Place a 1 μ F, X5R, capacitor between AVIN and AGND |
| 60 | AGND | G | Analog ground. This is the ground return for the controller. All AGND pins need to be connected to a quiet ground. |
| 61 | M/S | | A logic level low configures the device as Master and a logic level high configures the device as a Slave. Connect to ground in standalone mode. |
| 62 | VFB | I/O | External feedback input. The feedback loop is closed through this pin. A voltage divider at VOUT is used to set the output voltage. The mid-point of the divider is connected to VFB. A phase lead network from this pin to VOUT is also required to stabilize the loop. |
| 63 | EAIN | I | Optional error amplifier input. Allows for customization of the control loop for performance optimization. Leave this pin floating if not used. |
| 64 | SS | I/O | Soft-start node. The soft-start capacitor is connected between this pin and AGND. The value of this capacitor determines the startup time. See Soft-Start Operation in the Functional Description section for details. |
| 65 | RCLX | I/O | Short circuit protection. Connect a 100k resistor from RCLX to ground. |
| 66 | FQADJ | I/O | Adding a resistor (R_{FS}) to this pin will adjust the switching frequency of the EN2390QI. See Table 1 for suggested resistor values on R_{FS} for various PVIN/VOUT combinations to maximize efficiency. Do not leave this pin floating. |
| 68 | CGND | | Test pin. For Enpirion Internal Use Only. Connect to GND plane at all times. |
| 77 | PGND | | Not a perimeter pin. Device thermal pad to be connected to the system GND plane for heat-sinking purposes. |
| | | | |

Absolute Maximum Ratings

CAUTION: Absolute Maximum ratings are stress ratings only. Functional operation beyond the recommended operating conditions is not implied. Stress beyond the absolute maximum ratings may impair device life. Exposure to absolute maximum rated conditions for extended periods may affect device reliability.

| PARAMETER | SYMBOL | MIN | MAX | UNITS |
|--|----------------------|------|-----------------|-------|
| Pin Voltages – PVIN, VOUT, PG | | -0.5 | 15 | V |
| Pin Voltages – ENABLE, POK | | -0.5 | $AV_{IN} + 0.3$ | V |
| Pin Voltages – AVINO, AVIN, ENABLE, S_IN, S_OUT, M/S | | -0.5 | 6.0 | V |
| Pin Voltages – VFB, SS, EAIN, RCLX, FQADJ, VDDB, BTMP | | -0.5 | 2.75 | V |
| Dual Supply PVIN Rising and Falling Slew Rate (Note 1) | | 0.3 | 25 | V/ms |
| Single Supply PVIN Rising and Falling Slew Rate (Note 1) | | 0.3 | 6 | V/ms |
| Maximum Continuous Output Current | $I_{OUT_CONT_MAX}$ | | 14 | A |
| Storage Temperature Range | T_{STG} | -65 | 150 | °C |
| Maximum Operating Junction Temperature | T_{J-ABS_Max} | | 150 | °C |
| Reflow Temp, 10 Sec, MSL3 JEDEC J-STD-020A | | | 260 | °C |
| ESD Rating (based on Human Body Model) | | | 2000 | V |

Recommended Operating Conditions

| PARAMETER | SYMBOL | MIN | MAX | UNITS |
|---------------------------------|-----------|------|------|-------|
| Input Voltage Range | PVIN | 4.5 | 14 | V |
| AVIN: Controller Supply Voltage | AVIN | 2.5 | 5.5 | V |
| Output Voltage Range (Note 2) | V_{OUT} | 0.75 | 3.3 | V |
| Output Current | I_{OUT} | 0 | 9 | A |
| Operating Ambient Temperature | T_A | -40 | +85 | °C |
| Operating Junction Temperature | T_J | -40 | +125 | °C |

Thermal Characteristics

| PARAMETER | SYMBOL | TYP | UNITS |
|--|---------------|-----|-------|
| Thermal Resistance: Junction to Ambient (0 LFM) (Note 3) | θ_{JA} | 15 | °C/W |
| Thermal Resistance: Junction to Case (0 LFM) | θ_{JC} | 1.5 | °C/W |
| Thermal Shutdown | T_{SD} | 160 | °C |
| Thermal Shutdown Hysteresis | T_{SDH} | 35 | °C |

Note 1: PVIN rising and falling slew rates cannot be outside of specification. For accurate power up sequencing, use a fast ENABLE logic ($>3V/100\mu s$) after both AVIN and PVIN are high.

Note 2: Dropout: Maximum $V_{OUT} \leq V_{IN} - 2.5V$

Note 3: Based on 2oz. external copper layers and proper thermal design in line with EIJ/JEDEC JESD51-7 standard for high thermal conductivity boards.

Electrical Characteristics

NOTE: $V_{IN}=12V$, Minimum and Maximum values are over operating ambient temperature range unless otherwise noted. Typical values are at $T_A = 25^{\circ}C$.

| PARAMETER | SYMBOL | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
|--|----------------------|---|-------|---------------|---------------|---------|
| Operating Input Voltage | PVIN | | 4.5 | | 14.0 | V |
| Controller Input Voltage | AVIN | | 2.5 | | 5.5 | V |
| AVIN Under Voltage Lock-out rising | $AVIN_{UVLO\,R}$ | Voltage above which UVLO is not asserted | | 2.3 | | V |
| AVIN Under Voltage Lock-out falling | $AVIN_{OVLO\,F}$ | Voltage below which UVLO is asserted | | 2.1 | | V |
| AVIN pin Input Current | I_{AVIN} | | | 11 | | mA |
| Internal Linear Regulator Output Voltage | AVINO | | | 3.4 | | V |
| Shut-Down Supply Current | $IPVIN_S$ | $PVIN=12V$, $AVIN=3.4V$, $ENABLE=0V$ | | 300 | | μA |
| | I_{AVIN_S} | $PVIN=12V$, $AVIN=3.4V$, $ENABLE=0V$ | | 50 | | μA |
| Feedback Pin Voltage | V_{FB} | Feedback node voltage at: $V_{IN} = 12V$, $I_{LOAD} = 0$, $T_A = 25^{\circ}C$ Only | 0.594 | 0.60 | 0.606 | V |
| Feedback Pin Voltage | V_{FB} | Feedback node voltage at: $4.5V \leq V_{IN} \leq 14V$ $0A \leq I_{LOAD} \leq 9A$, $T_A = -40$ to $85^{\circ}C$ | 0.588 | 0.60 | 0.612 | V |
| Feedback pin Input Leakage Current | I_{FB} | VFB pin input leakage current (Note 4) | -5 | | 5 | nA |
| V_{OUT} Rise Time | t_{RISE} | $C_{SS} = 47nF$ (Note 4, Note 5, Note 6) | 1.96 | 2.8 | 3.64 | ms |
| Soft Start Capacitor Range | C_{SS_RANGE} | | 10 | 47 | 68 | nF |
| Continuous Output Current | $I_{OUT_MAX_CONT}$ | Subject to thermal derating | 0 | | 9 | A |
| ENABLE Logic High | V_{ENABLE_HIGH} | $4.5V \leq V_{IN} \leq 14V$; | 1.25 | | AV_{IN} | V |
| ENABLE Logic Low | V_{ENABLE_LOW} | $4.5V \leq V_{IN} \leq 14V$; | 0 | | 0.95 | V |
| ENABLE Lockout Time | $T_{ENLOCKOUT}$ | | | 8 | | ms |
| ENABLE pin Input Current | I_{ENABLE} | $AVIN = 5.5V$ $ENABLE = 1.8V$; $ENABLE = 3.3V$; $ENABLE = 5.5V$; | | 5 11 23 | 8 18 32 | μA |
| Switching Frequency | F_{SW} | $R_{FS} = 3.01k\Omega$ | | 1.0 | | MHz |
| External SYNC Clock Frequency Lock Range | F_{PLL_LOCK} | Range of SYNC clock frequency (See Table 1) | 0.8 | | 1.8 | MHz |
| S_IN Threshold – Low | $V_{S_IN_LO}$ | S_IN Clock Logic Low Level (Note 3) | | | 0.8 | V |
| S_IN Threshold – High | $V_{S_IN_HI}$ | S_IN Clock Logic High Level (Note 3) | 1.8 | | 2.5 | V |
| S_OUT Threshold – Low | $V_{S_OUT_LO}$ | S_OUT Clock Logic Low Level (Note 3) | | | 0.8 | V |
| S_OUT Threshold – | $V_{S_OUT_HI}$ | S_OUT Clock Logic High Level | 1.8 | | 2.5 | V |

| PARAMETER | SYMBOL | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
|----------------------------------|--------------|--|-----|-----------|------|---------|
| High | | (Note 3) | | | | |
| POK Lower Threshold | POK_{LT} | Percentage of Nominal Output Voltage for POK to be Low | | 90 | | % |
| POK Output low Voltage | V_{POKL} | With 4mA Current Sink into POK | | | 0.4 | V |
| POK Output Hi Voltage | V_{POKH} | PVIN Range: $4.5V \leq V_{IN} \leq 14V$ | | | AVIN | V |
| POK pin V_{OH} leakage current | I_{POKL} | POK High (Note 3) | | | 1 | μA |
| M/S Pin Logic Low | V_{T-LOW} | Tie Pin to GND | | | 0.8 | V |
| M/S Pin Logic High | V_{T-HIGH} | Pull up to AVIN Through an External Resistor REXT | 1.8 | | | V |
| M/S Pin Input Current | $I_{M/S}$ | REXT = 15k Ω ; AVIN = 3.4V; AVIN = 5.5V; | | 65 175 | | μA |

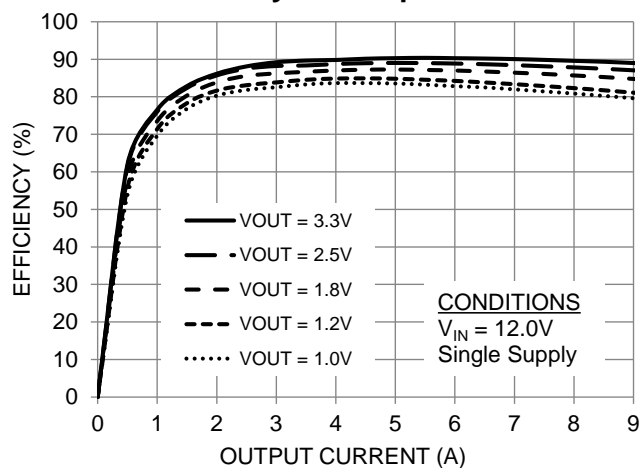
Note 4: Parameter not production tested but is guaranteed by design.

Note 5: Rise time calculation begins when $AVIN > V_{UVLO}$ and $ENABLE = HIGH$.

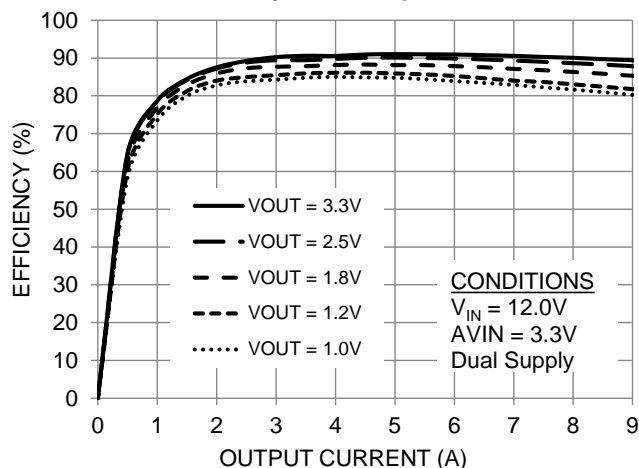
Note 6: V_{OUT} Rise Time Accuracy does not include soft-start capacitor tolerance.

Typical Performance Curves

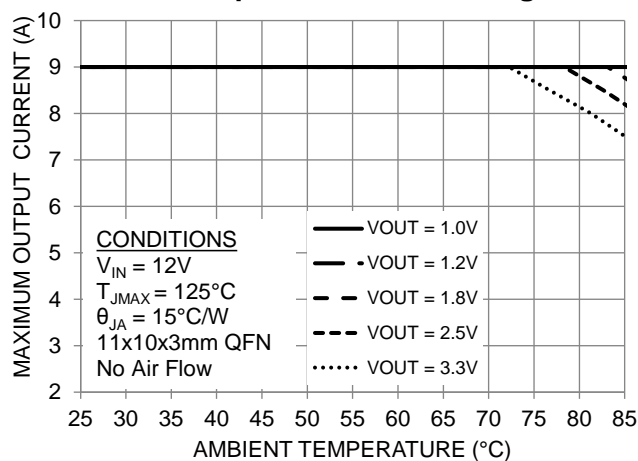
Efficiency vs. Output Current



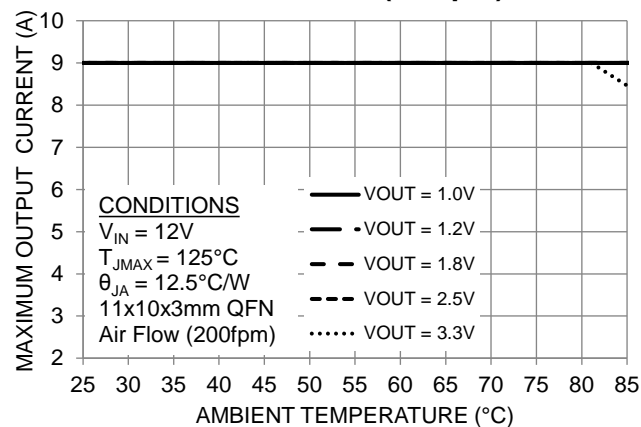
Efficiency vs. Output Current



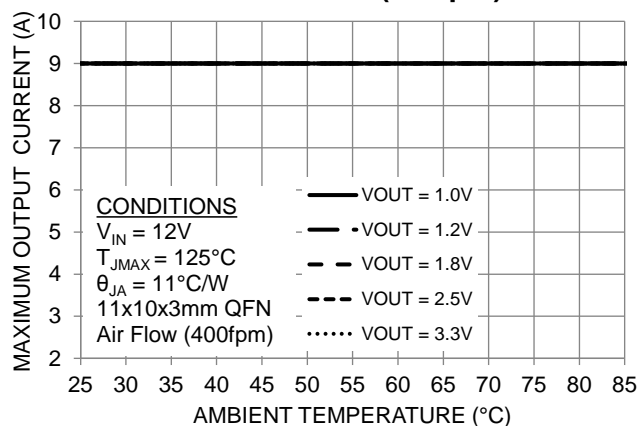
Output Current De-rating



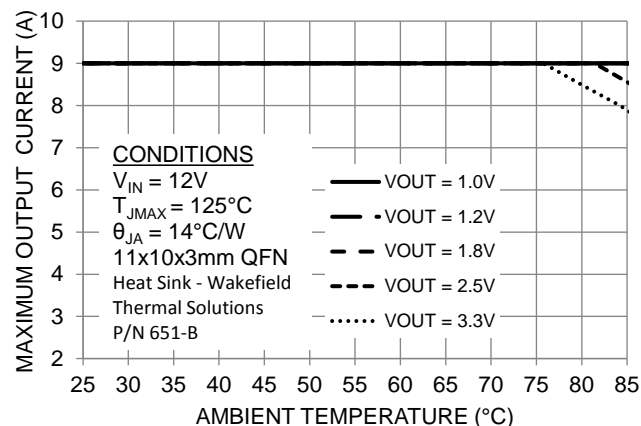
Output Current De-rating with Air Flow (200fpm)



Output Current De-rating with Air Flow (400fpm)

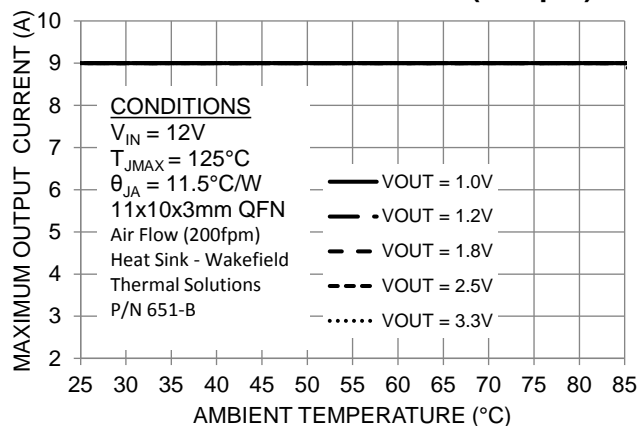


Output Current De-rating with Heat Sink

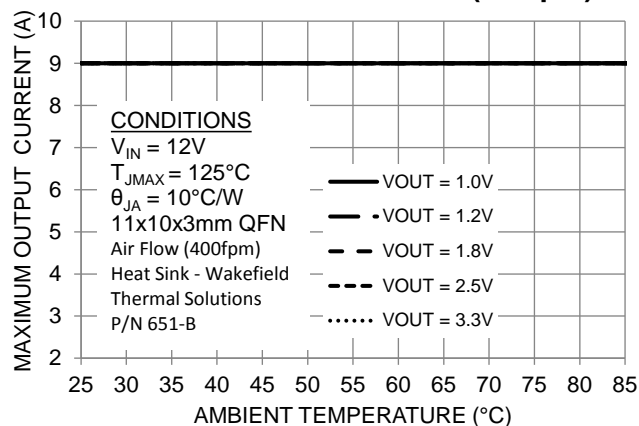


Typical Performance Curves

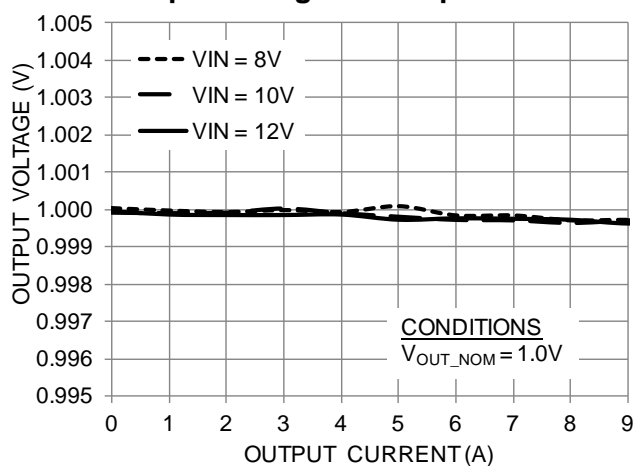
**Output Current De-rating
w/ Heat Sink and Air Flow (200fpm)**



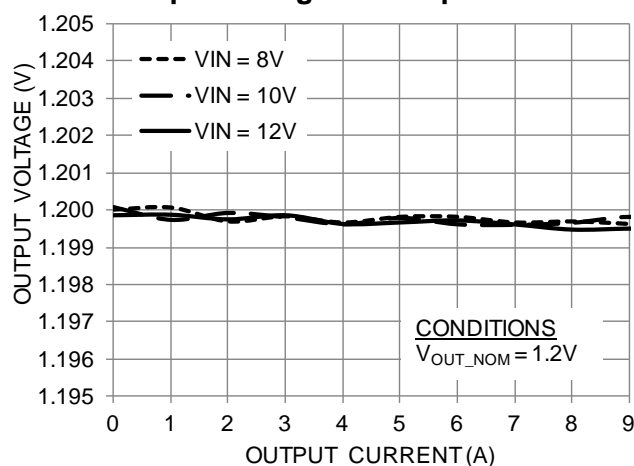
**Output Current De-rating
w/ Heat Sink and Air Flow (400fpm)**



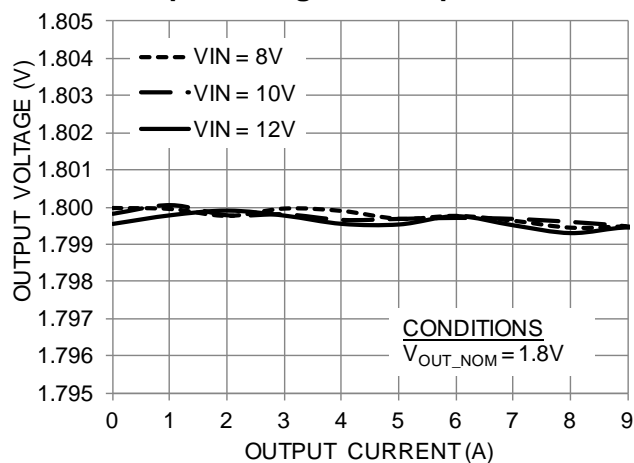
Output Voltage vs. Output Current



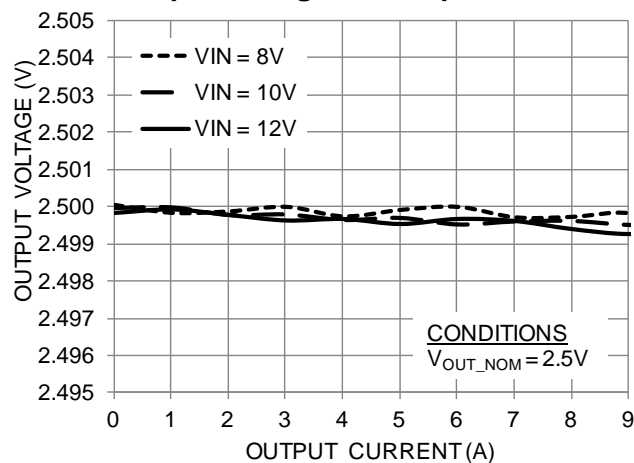
Output Voltage vs. Output Current



Output Voltage vs. Output Current

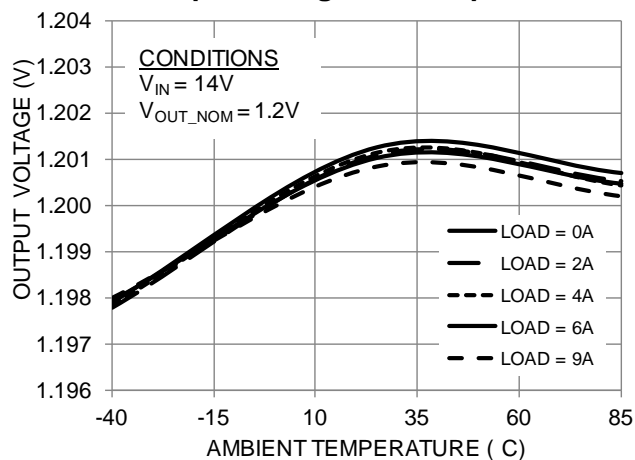


Output Voltage vs. Output Current

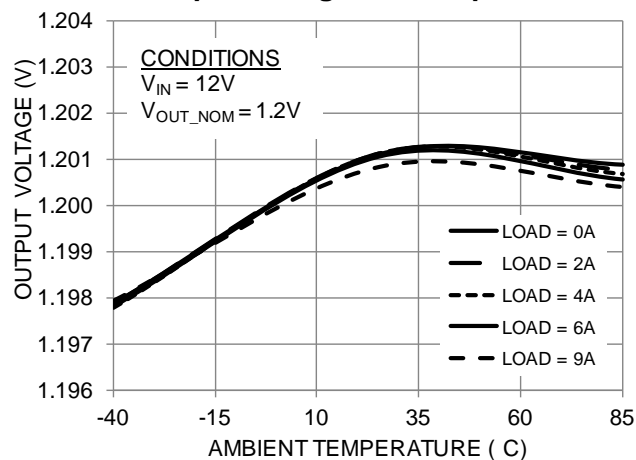


Typical Performance Curves

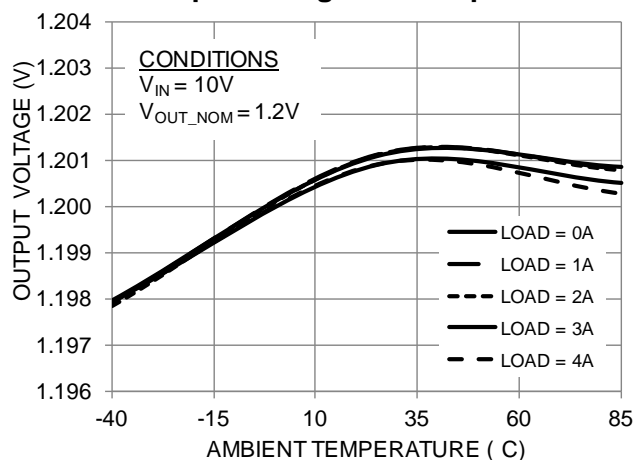
Output Voltage vs. Temperature



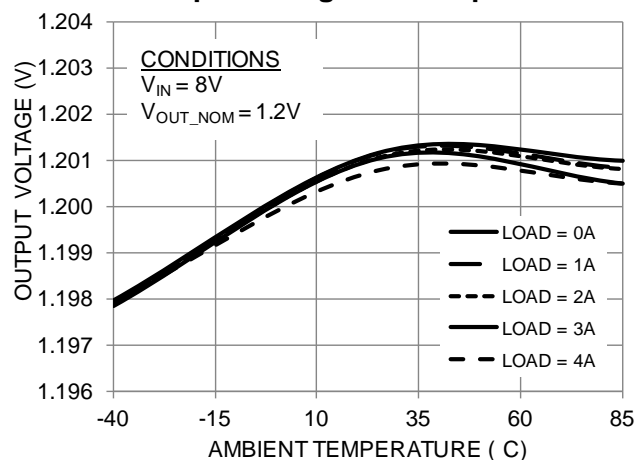
Output Voltage vs. Temperature



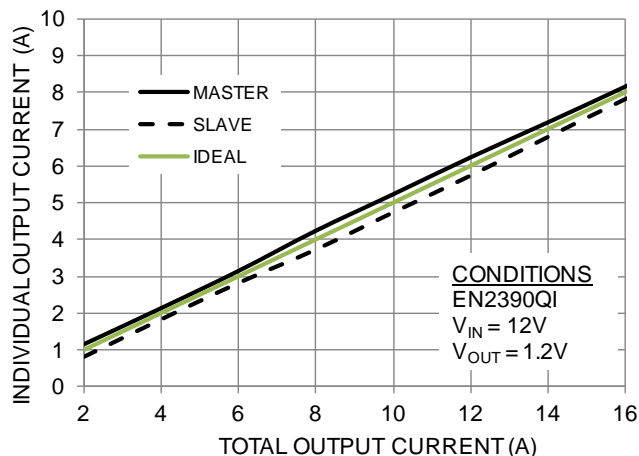
Output Voltage vs. Temperature



Output Voltage vs. Temperature

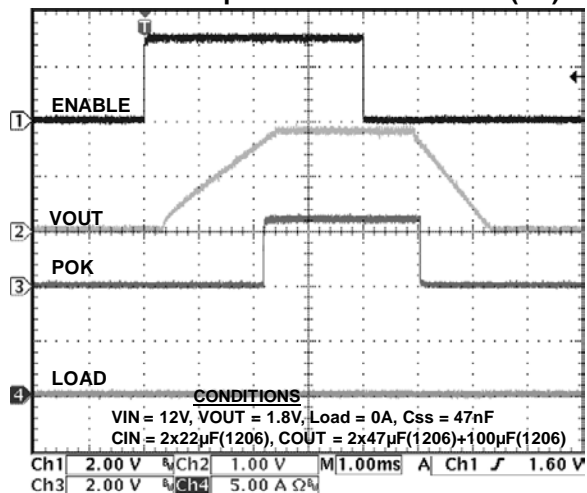


Parallel Current Share Breakdown

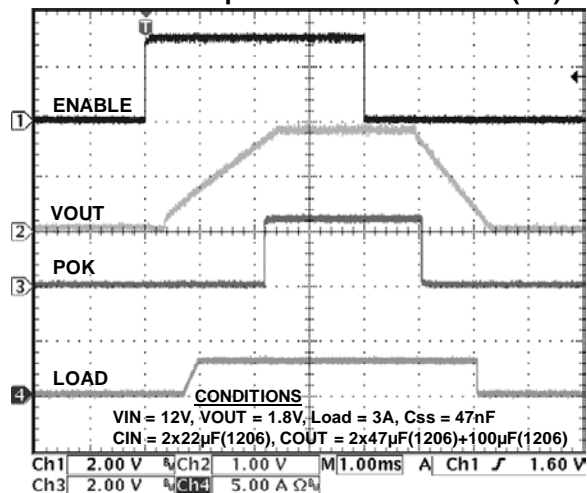


Typical Performance Characteristics

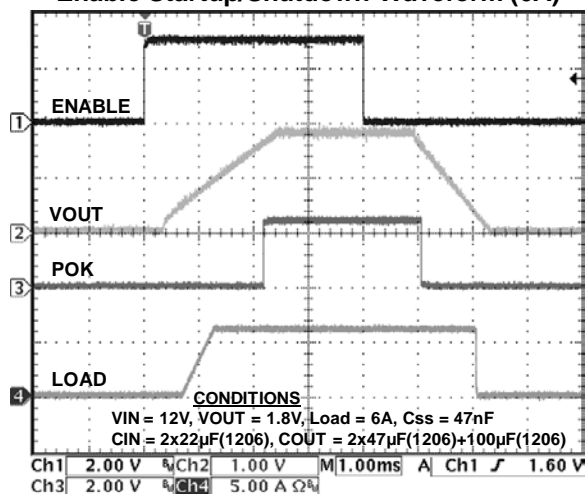
Enable Startup/Shutdown Waveform (0A)



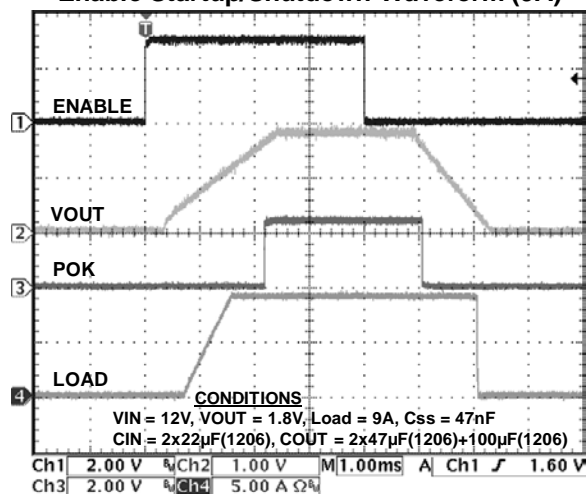
Enable Startup/Shutdown Waveform (3A)



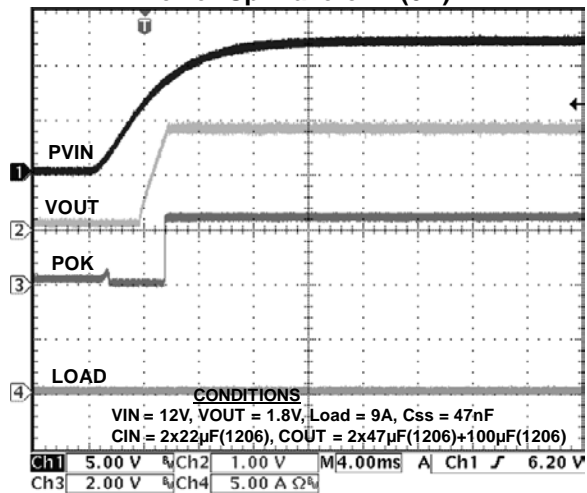
Enable Startup/Shutdown Waveform (6A)



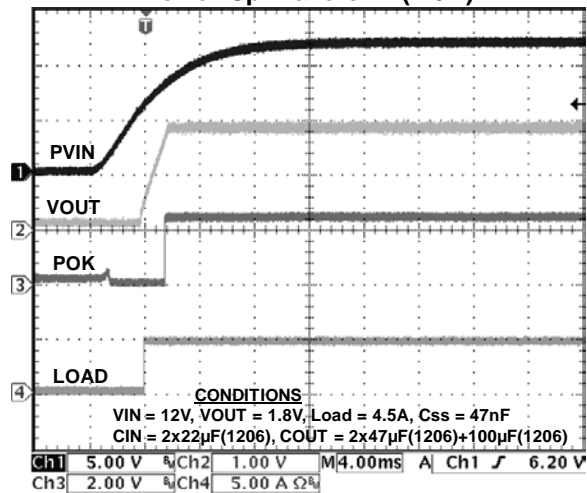
Enable Startup/Shutdown Waveform (9A)



Power Up Waveform (0A)

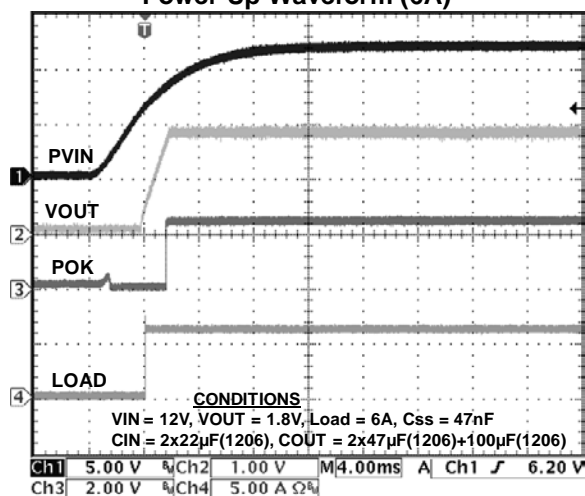


Power Up Waveform (4.5A)

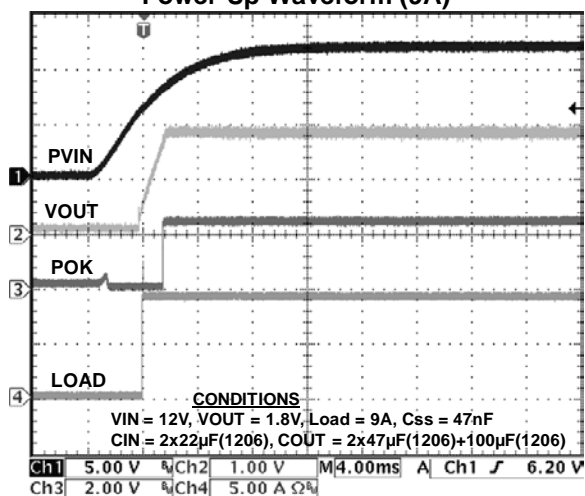


Typical Performance Characteristics

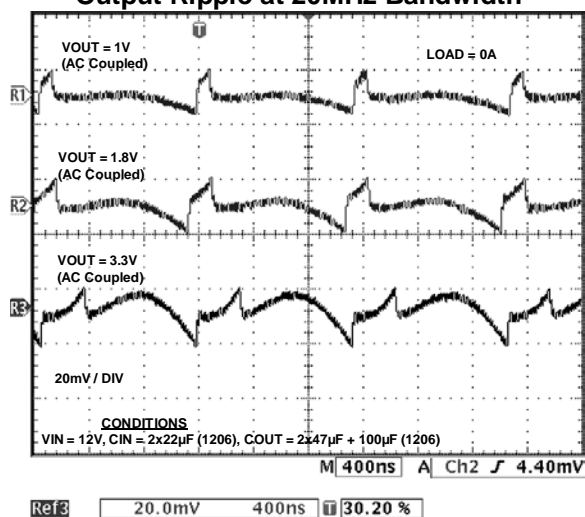
Power Up Waveform (6A)



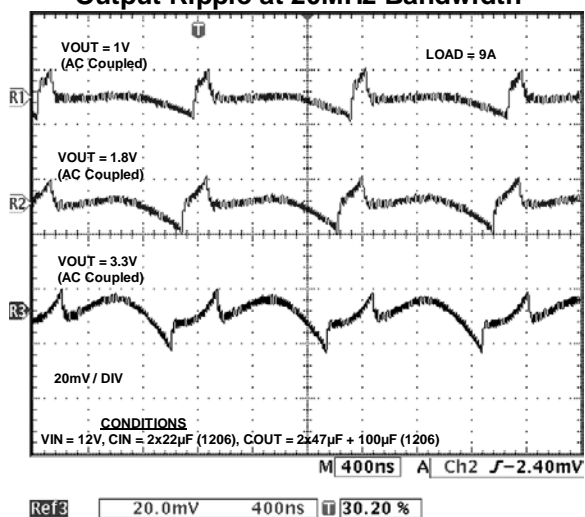
Power Up Waveform (9A)



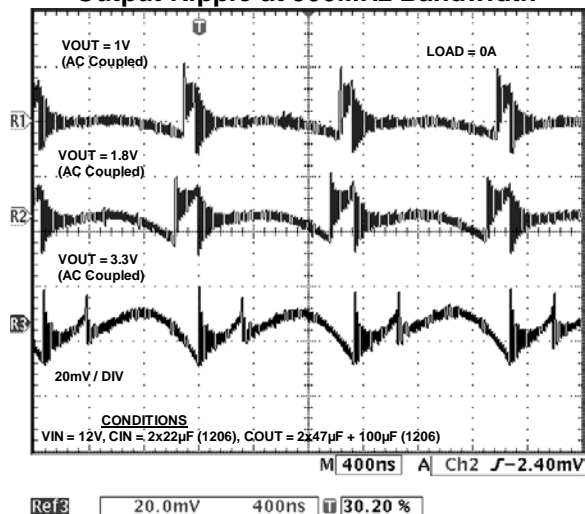
Output Ripple at 20MHz Bandwidth



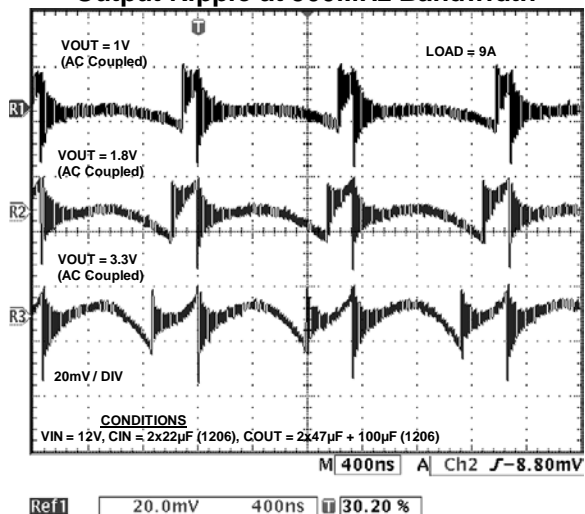
Output Ripple at 20MHz Bandwidth



Output Ripple at 500MHz Bandwidth

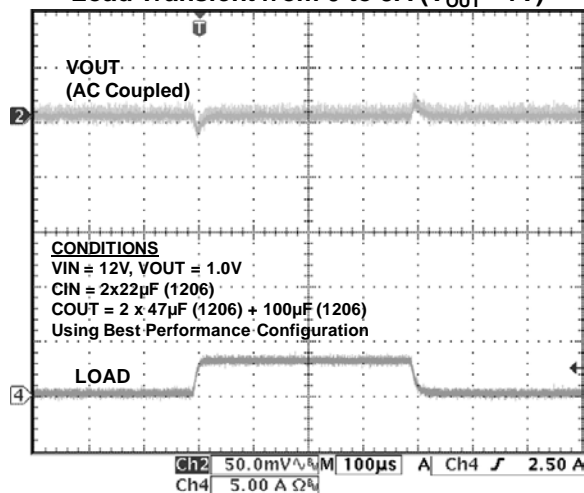


Output Ripple at 500MHz Bandwidth

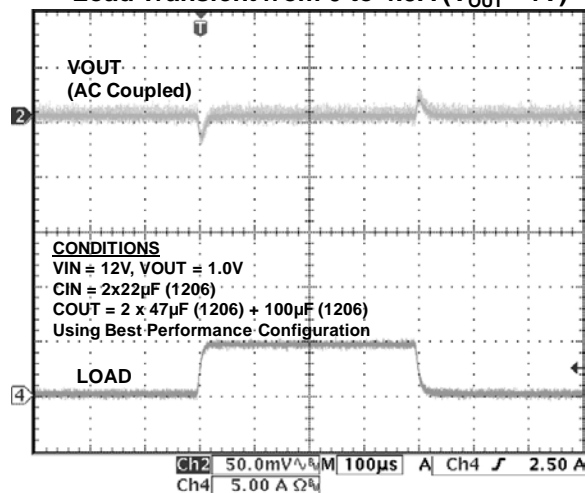


Typical Performance Characteristics

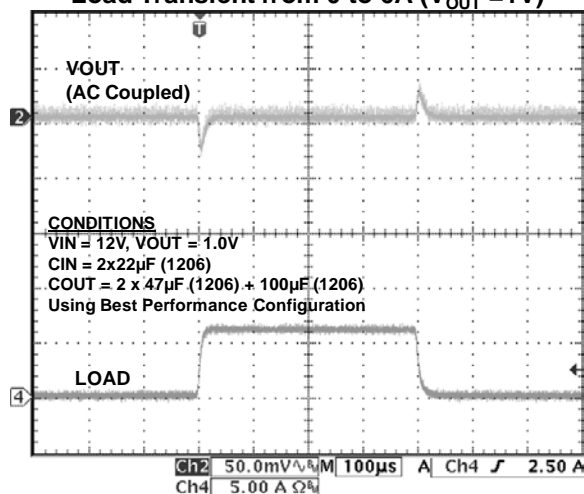
Load Transient from 0 to 3A ($V_{OUT} = 1V$)



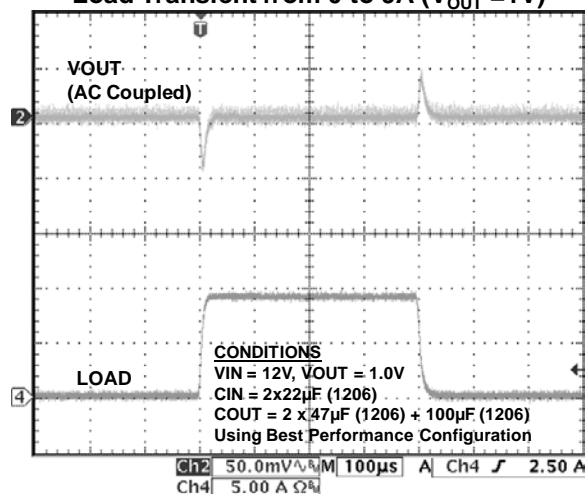
Load Transient from 0 to 4.5A ($V_{OUT} = 1V$)



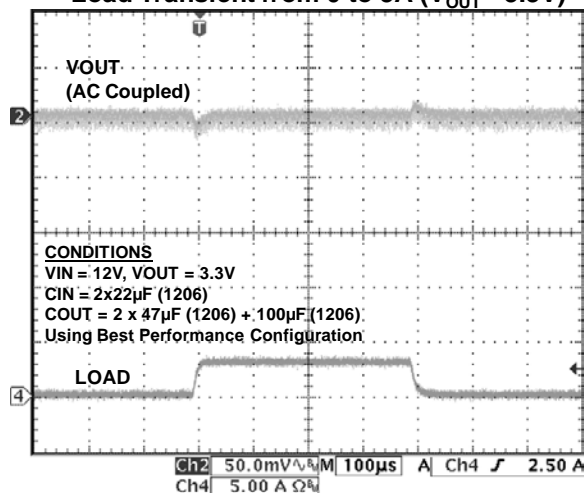
Load Transient from 0 to 6A ($V_{OUT} = 1V$)



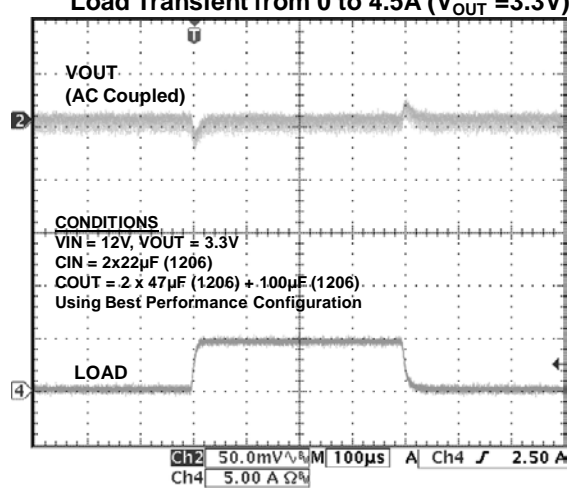
Load Transient from 0 to 9A ($V_{OUT} = 1V$)



Load Transient from 0 to 3A ($V_{OUT} = 3.3V$)

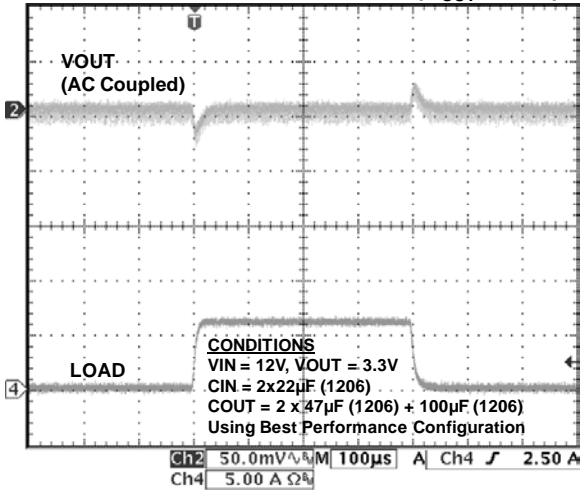


Load Transient from 0 to 4.5A ($V_{OUT} = 3.3V$)

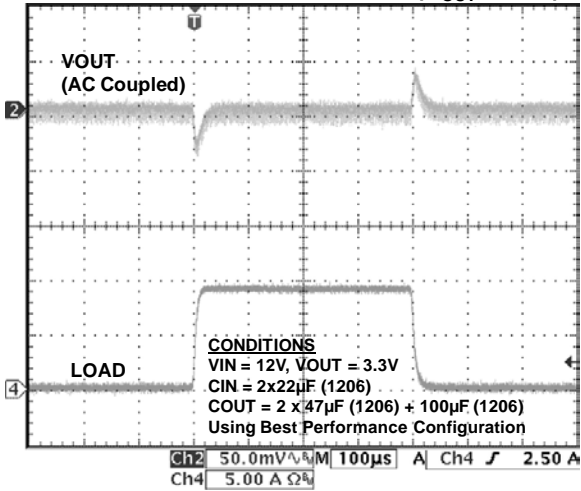


Typical Performance Characteristics

Load Transient from 0 to 6A ($V_{OUT} = 3.3V$)



Load Transient from 0 to 9A ($V_{OUT} = 3.3V$)



Functional Block Diagram

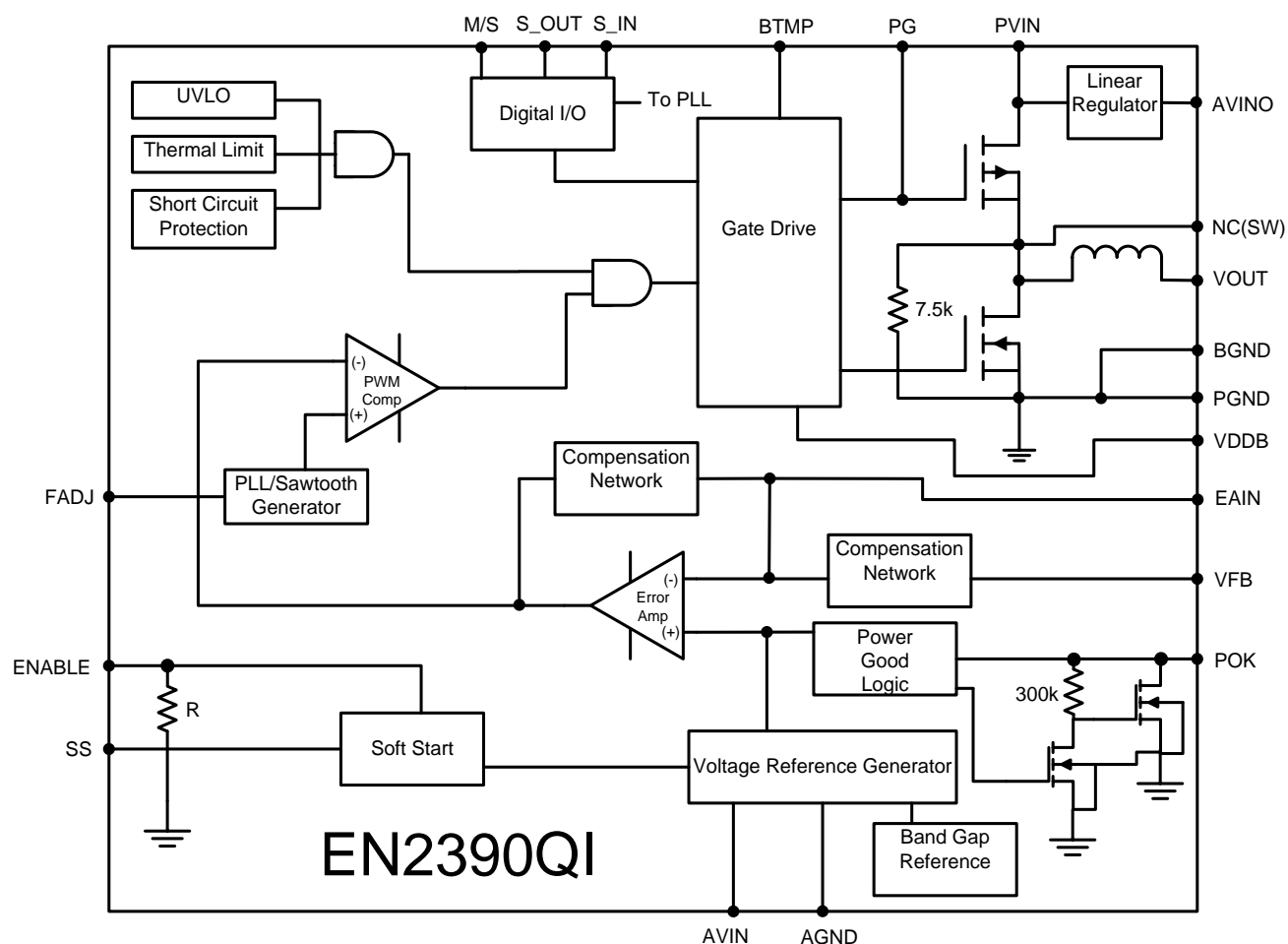


Figure 4: Functional Block Diagram

Functional Description

Synchronous Buck Converter

The EN2390QI is a highly integrated synchronous, buck converter with integrated controller, power MOSFET switches and integrated inductor. The nominal input voltage (PVIN) range is 4.5V to 14V and can support up to 9A of continuous output current. The output voltage is programmed using an external resistor divider network. The control loop utilizes a Type IV Voltage-Mode compensation network and maximizes on a low-noise PWM topology. Much of the compensation circuitry is internal to the device. However, a phase lead capacitor is required along with the output voltage feedback resistor divider to complete the Type IV compensation network. The high switching frequency of the EN2390QI enables the use of

small size input and output filter capacitors, as well as a wide loop bandwidth within a small foot print.

Protection Features:

The power supply has the following protection features:

- Short Circuit Protection
- Thermal Shutdown with Hysteresis.
- AVIN Under-Voltage Lockout Protection

Additional Features:

- Switching Frequency Synchronization.
- Programmable Soft-Start
- Power OK Output Monitoring

Power Up Sequence

The EN2390QI is designed to be powered by either a single input supply (PVIN) or two separate supplies: one for PVIN and the other for AVIN. The EN2390QI is not “hot pluggable.” Refer to the PVIN Slew Rate specification on page 4.

Single Input Supply Application (PVIN):

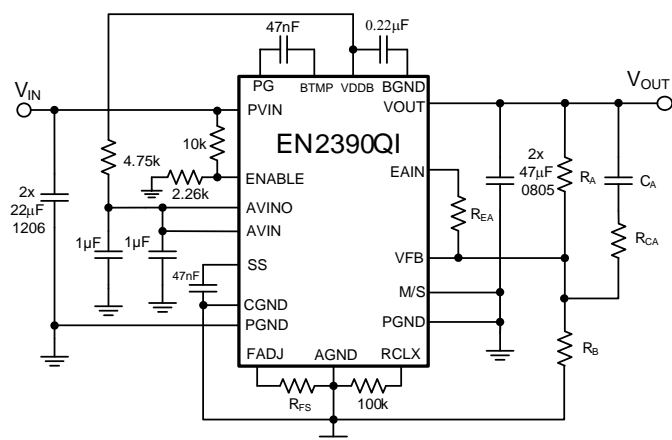


Figure 5: Single Input Supply Schematic

The EN2390QI has an internal linear regulator that converts PVIN to 3.4V. The output of the linear regulator is provided on the AVINO pin once the device is enabled. AVINO should be connected to AVIN on the EN2390QI. In this application, the following external components are required: Place a 1µF, X5R/X7R capacitor between AVINO and AGND as close as possible to AVINO. Place a 1µF, X5R/X7R capacitor between AVIN and AGND as close as possible to AVIN. In addition, place a resistor (R_{VB}) between VDDDB and AVIN, as shown in Figure 5. Altera recommends $R_{VB}=4.75k\Omega$. In this application, ENABLE cannot be asserted before PVIN. See diagram below for a recommended startup and shutdown sequencing.

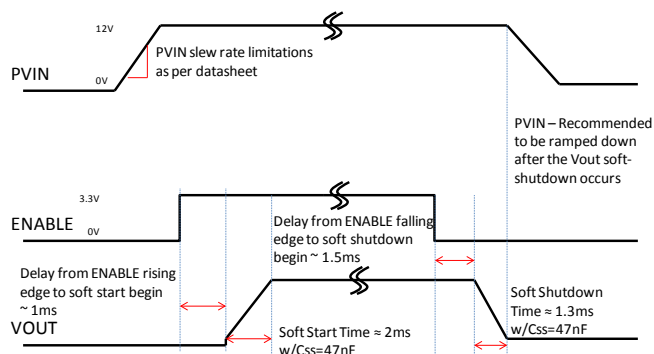


Figure 6: Single Supply Startup/Shutdown Sequence

If no external enable signal is used, a resistor divider (see Figure 5) from PVIN to ENABLE and then to ground can be used to enable and disable

the device at a programmed PVIN voltage level. The lower resistor (2.26k) can be adjusted to set startup and shutdown at a specific PVIN voltage level. In this operating mode the minimum PVIN is 6.8V due to the ENABLE threshold. See ENABLE and DISABLE thresholds in the Electrical Characteristics table.

Dual Input Supply Application (PVIN and AVIN):

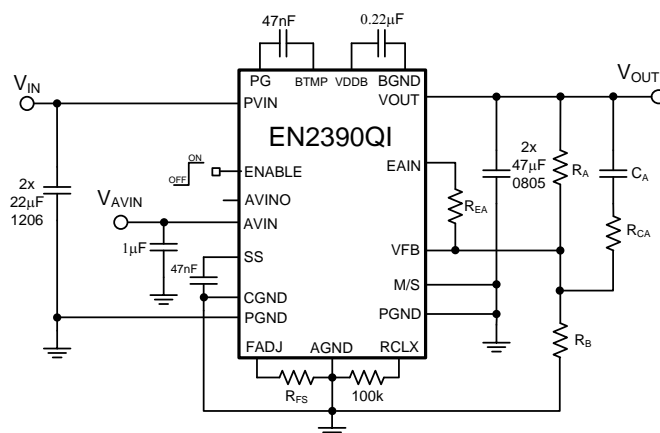


Figure 7: Dual Input Supply Schematic

In this application, place a 1µF, X5R/X7R, capacitor between AVIN and AGND as close as possible to AVIN. Refer to Figure 7 for a recommended schematic for a dual input supply application.

For dual input supply applications, the sequencing of the two input supplies, PVIN and AVIN, is very important. There are two common acceptable turn-on sequences for the device. AVIN can always come up before PVIN. If PVIN comes up before AVIN, then ENABLE must be toggled last, after AVIN is asserted. Do not turn off AVIN before PVIN and ENABLE during shutdown. Doing so will disable the internal controller while there may still be energy in the system. The device will not soft-shutdown properly and damage may occur. See diagram below for a recommended startup and shutdown sequencing.

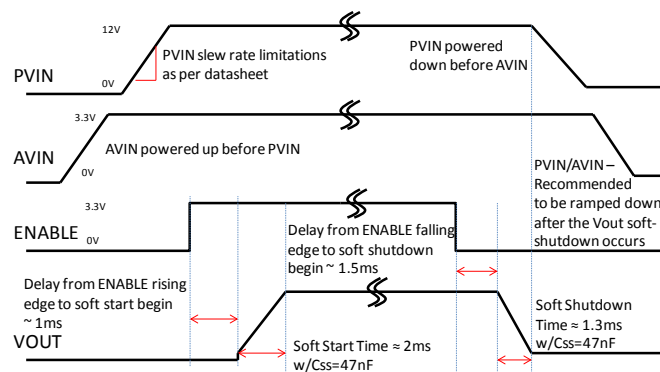


Figure 8: Dual Supply Startup/Shutdown Sequencing

Enable Operation

The ENABLE pin provides a means to enable normal operation or to shut down the device. A logic high will enable the converter into normal operation. When the ENABLE pin is asserted (high) the device will undergo a normal soft-start. A logic low will disable the converter. A logic low will power down the device in a controlled manner and the device is subsequently shut down. The ENABLE signal has to be low for at least the ENABLE Lockout Time (8ms) in order for the device to be re-enabled. To ensure accurate startup sequencing the ENABLE/DISABLE signal should be faster than 1V/100 μ s. A slower ENABLE/DISABLE signal may result in a delayed startup and shutdown response. Do not leave ENABLE floating.

Pre-Bias Operation

The EN2390QI is not designed to be turned on into a pre-biased output voltage. Be sure the output capacitors are not charged or the output of the EN2390QI is not pre-biased when the EN2390QI is first enabled.

Frequency Synchronization

The switching frequency of the EN2390QI can be phase-locked to an external clock source to move unwanted beat frequencies out of band. The internal switching clock of the EN2390QI can be phase locked to a clock signal applied to the S_{IN} pin. An activity detector recognizes the presence of an external clock signal and automatically phase-locks the internal oscillator to this external clock. Phase-lock will occur as long as the input clock frequency is in the range of 0.8MHz to 1.8MHz. The external clock frequency must be within $\pm 10\%$ of the nominal switching frequency set by the R_{FS} resistor. It is recommended to use a synchronized clock frequency close to the typical frequency recommendations in Table 1. A 3.01k Ω resistor from FQADJ to ground is recommended for clock frequencies within $\pm 10\%$ of 1MHz. When no clock is present, the device reverts to the free running frequency of the internal oscillator set by the R_{FS} resistor.

The efficiency performance of the EN2390QI for various P_{VIN}/V_{OUT} combinations can be optimized by adjusting the switching frequency. Table 1 shows recommended R_{FS} values for various P_{VIN}/V_{OUT} combinations in order to optimize performance of the EN2390QI.

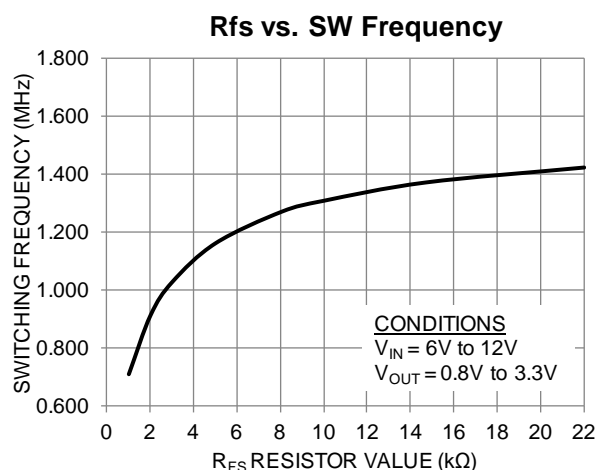


Figure 9. R_{FS} versus Switching Frequency

The efficiency performance of the EN2390QI for various V_{OUT}s can be optimized by adjusting the switching frequency. Table 1 shows recommended R_{FS} values for various V_{OUT}s in order to optimize performance of the EN2390QI.

| P _{VIN} | V _{OUT} | R _{FS} | Typical fsw |
|------------------|------------------|-----------------|-------------|
| 12V | 3.3V | 22k | 1.42 MHz |
| | 2.5V | 10k | 1.3 MHz |
| | 1.8V | 4.87k | 1.15 MHz |
| | 1.5V | 3.01k | 1.0 MHz |
| | 1.2V | 1.65k | 0.95 MHz |
| | <1.0V | 1.3k | 0.8 MHz |
| 5V | 2.5V | 22.1k | 1.4 MHz |
| | 1.8V | 10k | 1.3 MHz |
| | 1.5V | 6.65k | 1.25 MHz |
| | 1.2V | 4.87k | 1.15 MHz |
| | <1.0V | 3.01k | 1.0 MHz |

Table 1: Recommended R_{FS} Values

Soft-Start Operation

Soft start is a means to ramp the output voltage gradually upon start-up. The output voltage rise time is controlled by the choice of soft-start capacitor, which is placed between the SS pin and the AGND pin. During start-up of the converter, the reference voltage to the error amplifier is linearly increased to its final level by an internal current source of approximately 10 μ A. The soft-start time is measured from when V_{IN} > V_{UVLOR} and ENABLE pin voltage crosses its logic high threshold to when V_{OUT} reaches its programmed value. The total soft-start time can be calculated by:

$$\text{Soft Start Time (ms): } T_{SS} \approx C_{SS} [\text{nF}] \times 0.06$$

Typical soft-start time is approximately 2.8ms with SS capacitor value of 47nF.

POK Operation

The POK signal is an open drain signal (requires a pull up resistor to AVIN or similar voltage) from the converter indicating the output voltage is within the specified range. Typically, a 100kΩ or lower resistance is used as the pull-up resistor. The POK signal will be logic high (AVIN) when the output voltage is above 90% of the programmed voltage level. If the output voltage is below this point, the POK signal will be a logic low. The POK signal can be used to sequence down-stream converters by tying to their enable pins.

Short Circuit Protection

The short circuit protection feature will protect the device if the output is shorted to ground. Short circuit protection is achieved by sensing the current flowing through a sense PFET. When the sensed current exceeds the threshold for more than 32 cycles, both power FETs are turned off for the rest of the switching cycle. If the short circuit condition is removed, the device will reactivate soft-start and resume PWM operation. In the event the short circuit trips consistently in normal operation, the device enters a hiccup mode. While in hiccup mode, the device is disabled for a short while and restarted with a normal soft-start. The hiccup time is approximately 32ms. This cycle can continue indefinitely as long as the short circuit condition persists. Use a resistor value of 100k from the RCLX pin to ground to enable this feature.

Thermal Overload Protection

Thermal shutdown circuit will disable device operation when the junction temperature exceeds approximately 160°C. After a thermal shutdown event, when the junction temperature drops by approx 35°C, the converter will re-start with a normal soft-start.

AVIN Under-Voltage Lock-Out (UVLO)

Internal circuits ensure that the converter will not start switching until the AVIN input voltage is above the specified minimum voltage. Hysteresis, input de-glitch and output leading edge blanking ensures

high noise immunity and prevents false UVLO triggers.

Master / Slave (Parallel) Operation:

Up to four EN2390QI devices may be connected in a Master/Slave configuration to handle larger load currents. The maximum output current for each parallel device will need to be de-rated by 20 percent so that no devices will over current due to current mis-match. The Master device's switching clock may be phase-locked to an external clock source via the S_IN pin or left open and use its default switching frequency. The device is placed in Master mode by pulling the M/S pin low or in Slave mode by pulling M/S pin high. Note that the M/S pin is also pulled low for standalone mode. In Master mode, the internal PWM signal is output on the S_OUT pin. This PWM signal from the Master is fed to the Slave device at its S_IN input. The Slave device acts like an extension of the power FETs in the Master. The inductor in the Slave prevents crow-bar currents from Master to Slave due to timing delays. Parallel operation in dual supply mode is shown in Figure 11. Single supply mode operation may also be implemented similarly. Note that only critical components are shown. The red text and red lines indicate the important parallel operation connections and care should be taken in layout to ensure low impedance between those paths. The parallel current matching is illustrated in Figure 10.

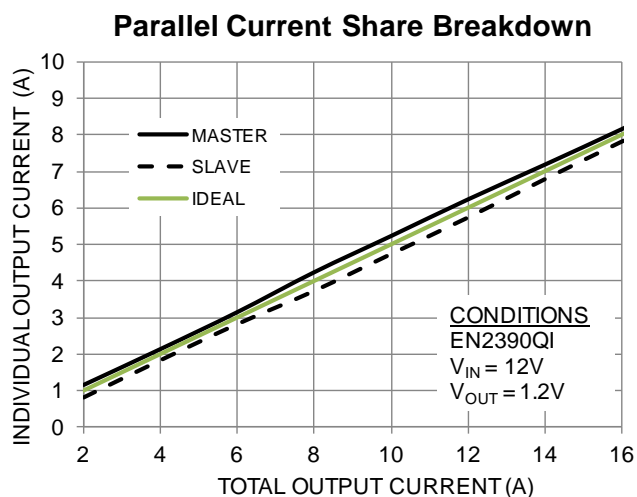


Figure 10. Parallel Current Matching

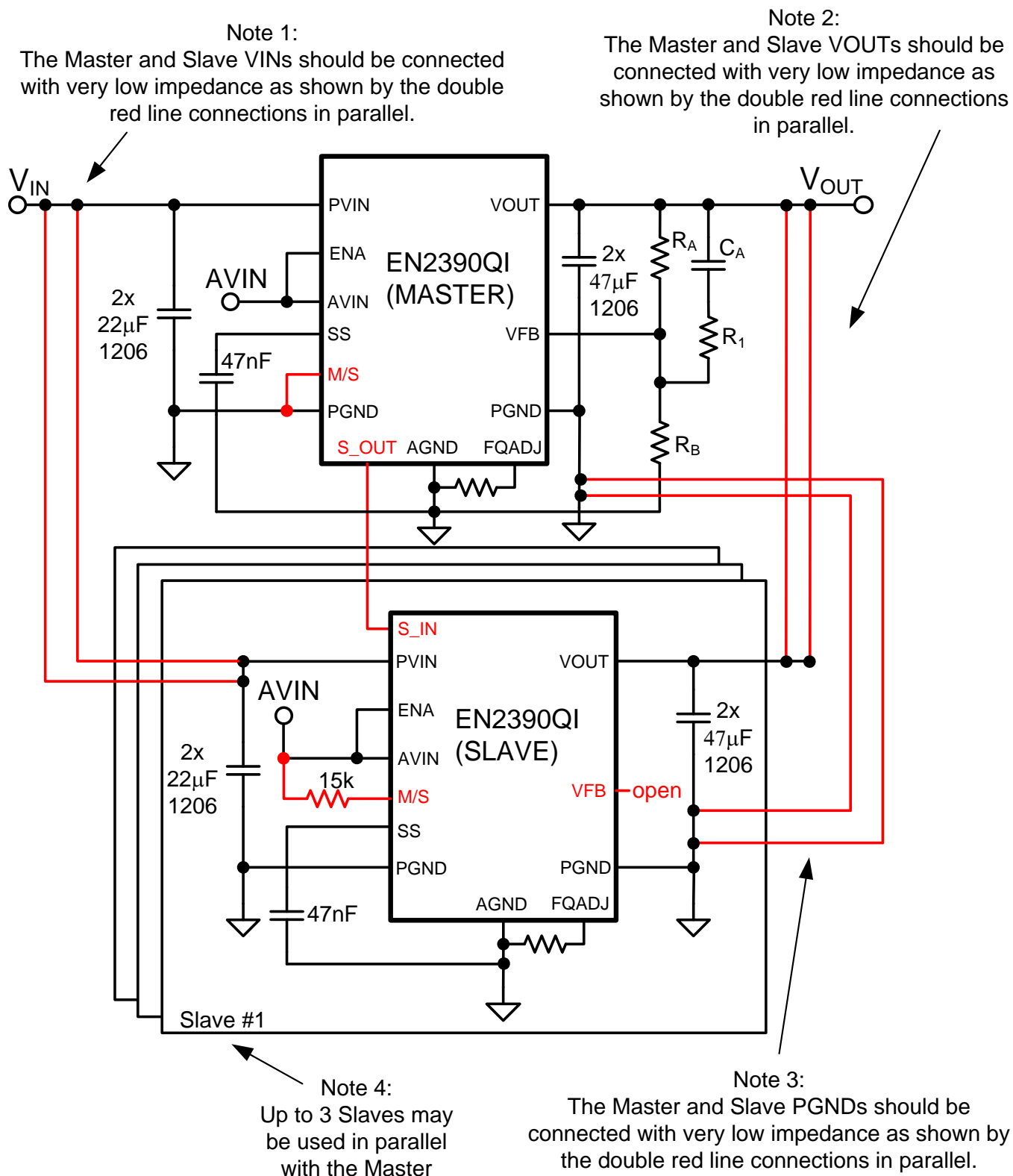


Figure 11. Parallel Operation Illustration

Application Information

Output Voltage Programming and Loop Compensation

The EN2390QI uses a Type IV Voltage Mode compensation network. Type IV Voltage Mode control is a proprietary Altera Enpirion control scheme that maximizes control loop bandwidth to deliver excellent load transient responses and maintain output regulation with pin point accuracy. For ease of use, most of this network has been customized and is integrated within the device package. The EN2390QI output voltage is programmed using a simple resistor divider network (R_A and R_B). The feedback voltage at VFB is nominally 0.6V. R_A is predetermined based on Table 4 and R_B can be calculated based on Figure 12. The values recommended for C_{OUT} , C_A , R_{CA} and R_{EA} make up the external compensation of the EN2390QI. It will vary with each PVIN and VOUT combination to optimize on performance. The EN2390QI solution can be optimized for either smallest size or highest performance. Please see Table 4 for a list of recommended R_A , C_A , R_{CA} , R_{EA} and C_{OUT} values for each solution.

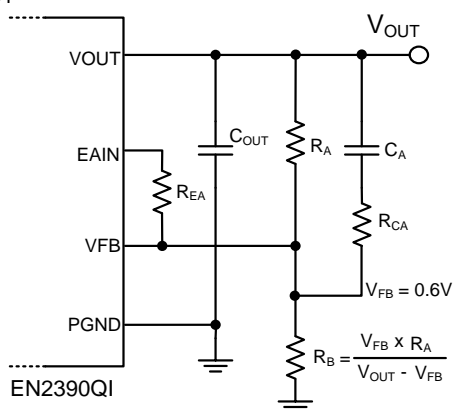


Figure 12: V_{OUT} Resistor Divider & Compensation Components. See Table 4 for details.

Input Capacitor Selection

The EN2390QI requires two 22 μ F/1206 input capacitors. Low-cost, low-ESR ceramic capacitors should be used as input capacitors for this converter. The dielectric must be X5R or X7R rated. **Y5V or equivalent dielectric formulations must not be used as these lose too much capacitance with frequency, temperature and bias voltage.** In some applications, lower value capacitors are needed in parallel with the larger, capacitors in order to provide high frequency decoupling. Table 2 contains a list of recommended input capacitors.

Recommended Input Capacitors

| Description | MFG | P/N |
|---------------------------------|-------------|-------------------|
| 22 μ F, 16V, X5R, 10%, 1206 | Murata | GRM31CR61C226ME15 |
| 22 μ F, 16V, X5R, 20%, 1206 | Taiyo Yuden | EMK316ABJ226ML-T |

Table 2: Recommended Input Capacitors

Output Capacitor Selection

As seen from Table 4, the EN2390QI has been optimized for use with one 100 μ F/1206 plus two 47 μ F/1206 output capacitors for best performance. For smallest solution size, various combinations of output capacitance may be used. See Table 4 for details. Low ESR ceramic capacitors are required with X5R or X7R rated dielectric formulation. **Y5V or equivalent dielectric formulations must not be used as these lose too much capacitance with frequency, temperature and bias voltage.** Table 4 contains a list of recommended output capacitors

Output ripple voltage is determined by the aggregate output capacitor impedance. Capacitor impedance, denoted as Z, is comprised of capacitive reactance, effective series resistance, ESR, and effective series inductance, ESL reactance.

Placing output capacitors in parallel reduces the impedance and will hence result in lower ripple voltage.

$$\frac{1}{Z_{Total}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \dots + \frac{1}{Z_n}$$

Recommended Output Capacitors

| Description | MFG | P/N |
|-----------------------------------|-------------|--------------------|
| 47 μ F, 6.3V, X5R, 20%, 1206 | Murata | GRM31CR60J476ME19L |
| 47 μ F, 10V, X5R, 20%, 1206 | Taiyo Yuden | LMK316BJ476ML-T |
| 22 μ F, 10V, X5R, 20%, 0805 | Panasonic | ECJ-2FB1A226M |
| 22 μ F, 10V, X5R, 20%, 0805 | Taiyo Yuden | LMK212BJ226MG-T |
| 100 μ F, 6.3V, X5R, 20%, 1206 | Murata | GRM31CR60J107ME39L |
| | Taiyo Yuden | JMK316BJ107ML-T |

Table 3: Recommended Output Capacitors

| Best Performance | | | | | | | Smallest Solution Size | | | | | | |
|--|----------|---------------------|-------------------------------|-------------------------------|-------------|----------------|---|----------|---------------------|-------------------------------|-------------------------------|-------------|----------------|
| $C_{IN} = 2x22\mu F/1206$ | | | | | | | $C_{IN} = 2x22\mu F/1206$ | | | | | | |
| $C_{OUT} = 2x47\mu F/1206 + 100\mu F/1206$ | | | | | | | $V_{OUT} \leq 1.8V, C_{OUT} = 2x47\mu F/0805$ $1.8V < V_{OUT} \leq 5.0V, C_{OUT} = 2x47\mu F/1206$ | | | | | | |
| $R_A = 200\text{ k}\Omega$ | | | | | | | $R_A = 75k$ | | | | | | |
| PVIN (V) | VOUT (V) | C _A (pF) | R _{CA} (k Ω) | R _{EA} (k Ω) | Ripple (mV) | Deviation (mV) | PVIN (V) | VOUT (V) | C _A (pF) | R _{CA} (k Ω) | R _{EA} (k Ω) | Ripple (mV) | Deviation (mV) |
| 14V | 0.9V | 15 | 18 | 0 | 5.83 | 44 | 14V | 0.9V | 18 | 8.2 | Open | 15 | 93 |
| | 1.2V | 15 | 22 | 0 | 7.22 | 48 | | 1.2V | 18 | 8.2 | Open | 21 | 104 |
| | 1.5V | 18 | 22 | 0 | 8.63 | 38 | | 1.5V | 18 | 8.2 | Open | 27 | 110 |
| | 1.8V | 15 | 22 | 0 | 10.8 | 50 | | 1.8V | 18 | 8.2 | Open | 35 | 120 |
| | 2.5V | 27 | 5.1 | 33 | 14.6 | 72 | | 2.5V | 15 | 8.2 | Open | 54 | 150 |
| | 3.3V | 22 | 8.2 | 33 | 26.1 | 76 | | 3.3V | 10 | 8.2 | Open | 81 | 215 |
| 12V | 0.9V | 27 | 18 | 0 | 5.21 | 40 | 12V | 0.9V | 27 | 5.1 | Open | 15 | 96 |
| | 1.2V | 22 | 22 | 0 | 6.7 | 36 | | 1.2V | 27 | 5.1 | Open | 21 | 104 |
| | 1.5V | 18 | 22 | 0 | 8.98 | 44 | | 1.5V | 27 | 5.1 | Open | 27 | 112 |
| | 1.8V | 18 | 22 | 0 | 10 | 50 | | 1.8V | 27 | 5.1 | Open | 34 | 130 |
| | 2.5V | 27 | 5.1 | 33 | 12.6 | 76 | | 2.5V | 22 | 5.1 | Open | 52 | 162 |
| | 3.3V | 22 | 8.2 | 33 | 23.6 | 72 | | 3.3V | 15 | 5.1 | Open | 77 | 221 |
| 10V | 0.9V | 27 | 18 | 0 | 5.01 | 44 | 10V | 0.9V | 56 | 2 | Open | 15 | 99 |
| | 1.2V | 22 | 22 | 0 | 6.28 | 40 | | 1.2V | 56 | 2 | Open | 20 | 107 |
| | 1.5V | 18 | 22 | 0 | 8.57 | 54 | | 1.5V | 39 | 2 | Open | 26 | 122 |
| | 1.8V | 18 | 22 | 0 | 9.44 | 60 | | 1.8V | 39 | 2 | Open | 33 | 126 |
| | 2.5V | 33 | 5.1 | 33 | 11 | 64 | | 2.5V | 33 | 2 | Open | 50 | 169 |
| | 3.3V | 27 | 8.2 | 33 | 21.6 | 68 | | 3.3V | 22 | 2 | Open | 71 | 241 |
| 8V | 0.9V | 27 | 18 | 0 | 4.9 | 44 | 8V | 0.9V | 100 | 0 | Open | 15 | 108 |
| | 1.2V | 22 | 22 | 0 | 5.82 | 48 | | 1.2V | 100 | 0 | Open | 20 | 113 |
| | 1.5V | 22 | 22 | 0 | 7.48 | 56 | | 1.5V | 82 | 0 | Open | 25 | 122 |
| | 1.8V | 22 | 22 | 0 | 8.01 | 54 | | 1.8V | 68 | 0 | Open | 31 | 136 |
| | 2.5V | 33 | 5.1 | 33 | 10.7 | 76 | | 2.5V | 47 | 0 | Open | 46 | 183 |
| | 3.3V | 27 | 8.2 | 33 | 20.5 | 84 | | 3.3V | 33 | 0 | Open | 62 | 253 |
| 6.6V | 0.9V | 33 | 18 | 0 | 4.58 | 46 | 6.6V | 0.9V | 100 | 0 | Open | 14 | 121 |
| | 1.2V | 27 | 22 | 0 | 5.28 | 54 | | 1.2V | 100 | 0 | Open | 19 | 128 |
| | 1.5V | 27 | 22 | 0 | 6.44 | 54 | | 1.5V | 100 | 0 | Open | 24 | 138 |
| | 1.8V | 22 | 22 | 0 | 7.2 | 58 | | 1.8V | 100 | 0 | Open | 29 | 149 |
| | 2.5V | 33 | 5.1 | 33 | 11.4 | 84 | | 2.5V | 68 | 0 | Open | 41 | 188 |
| | 3.3V | 33 | 8.2 | 33 | 18.4 | 96 | | 3.3V | 47 | 0 | Open | 53 | 239 |
| 5V | 0.9V | 39 | 18 | 0 | 4.1 | 54 | 5V | 0.9V | 100 | 0 | Open | 13 | 152 |
| | 1.2V | 33 | 22 | 0 | 5.1 | 62 | | 1.2V | 100 | 0 | Open | 18 | 161 |
| | 1.5V | 27 | 22 | 0 | 6.2 | 66 | | 1.5V | 100 | 0 | Open | 22 | 177 |
| | 1.8V | 27 | 22 | 0 | 7.02 | 68 | | 1.8V | 100 | 0 | Open | 25 | 183 |
| | 2.5V | 39 | 5.1 | 33 | 9.84 | 104 | | 2.5V | 100 | 0 | Open | 33 | 216 |

Table 4: R_A , C_A , R_{CA} and R_{EA} Values for Various PVIN/VOUT Combinations: Best Performance vs. Smallest Solution Size. Use the equations in Figure 12 to calculate R_B . Output ripple is measured at no load and nominal deviation is for a 9A load transient step. For a voltage in between the specified output voltages, choose compensation values of the lower output voltage setting.

Thermal Considerations

Thermal considerations are important power supply design facts that cannot be avoided in the real world. Whenever there are power losses in a system, the heat that is generated by the power dissipation needs to be accounted for. The Altera Enpirion PowerSoC helps alleviate some of those concerns.

The Altera Enpirion EN2390QI DC-DC converter is packaged in a 10x11x3mm 76-pin QFN package. The QFN package is constructed with copper lead frames that have exposed thermal pads. The exposed thermal pad on the package should be soldered directly on to a copper ground pad on the printed circuit board (PCB) to act as a heat sink. The recommended maximum junction temperature for continuous operation is 125°C. Continuous operation above 125°C may reduce long-term reliability. The device has a thermal overload protection circuit designed to turn off the device at an approximate junction temperature value of 160°C.

The following example and calculations illustrate the thermal performance of the EN2390QI.

Example:

$$V_{IN} = 12V$$

$$V_{OUT} = 1.2V$$

$$I_{OUT} = 9A$$

First calculate the output power.

$$P_{OUT} = 1.2V \times 9A = 10.8W$$

Next, determine the input power based on the efficiency (η) shown in Figure 13.

$$\eta = P_{OUT} / P_{IN} = 82\% = 0.82$$

$$P_{IN} = P_{OUT} / \eta$$

$$P_{IN} \approx 10.8W / 0.8 \approx 13.17W$$

The power dissipation (P_D) is the power loss in the system and can be calculated by subtracting the output power from the input power.

$$P_D = P_{IN} - P_{OUT}$$

$$\approx 13.17W - 10.8W \approx 2.37W$$

With the power dissipation known, the temperature rise in the device may be estimated based on the θ_{JA} value (θ_{JA}). The θ_{JA} parameter estimates how much the temperature will rise in the device for every watt of power dissipation. The EN2390QI has a θ_{JA} value of 15 °C/W without airflow.

Determine the change in temperature (ΔT) based on P_D and θ_{JA} .

$$\Delta T = P_D \times \theta_{JA}$$

$$\Delta T \approx 2.37W \times 15^\circ C/W = 35.56^\circ C \approx 36^\circ C$$

The junction temperature (T_J) of the device is approximately the ambient temperature (T_A) plus the change in temperature. We assume the initial ambient temperature to be 25°C.

$$T_J = T_A + \Delta T$$

$$T_J \approx 25^\circ C + 36^\circ C \approx 61^\circ C$$

The maximum operating junction temperature (T_{JMAX}) of the device is 125°C, so the device can operate at a higher ambient temperature. The maximum ambient temperature (T_{AMAX}) allowed can be calculated.

$$T_{AMAX} = T_{JMAX} - P_D \times \theta_{JA}$$

$$\approx 125^\circ C - 36^\circ C \approx 89^\circ C$$

The maximum ambient temperature the device can reach is 89°C given the input and output conditions. Note that the efficiency will be slightly lower at higher temperatures and this calculation is an estimate. Check De-rating Curves for guaranteed maximum output current over temperature.

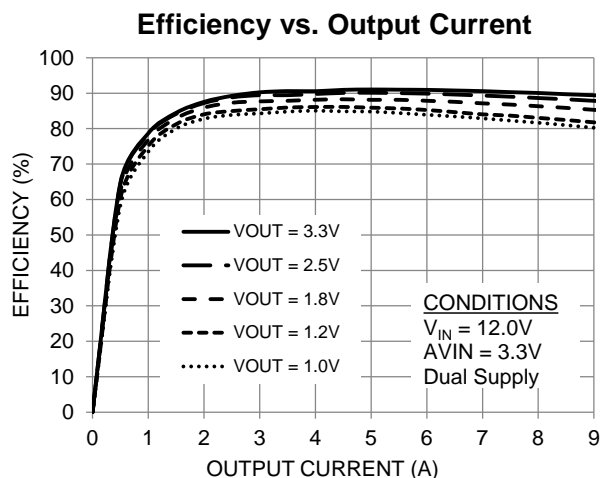


Figure 13: Efficiency vs. Output Current

For $V_{IN} = 12V$, $V_{OUT} = 1.2V$ at 9A, $\eta \approx 82\%$

Engineering Schematic

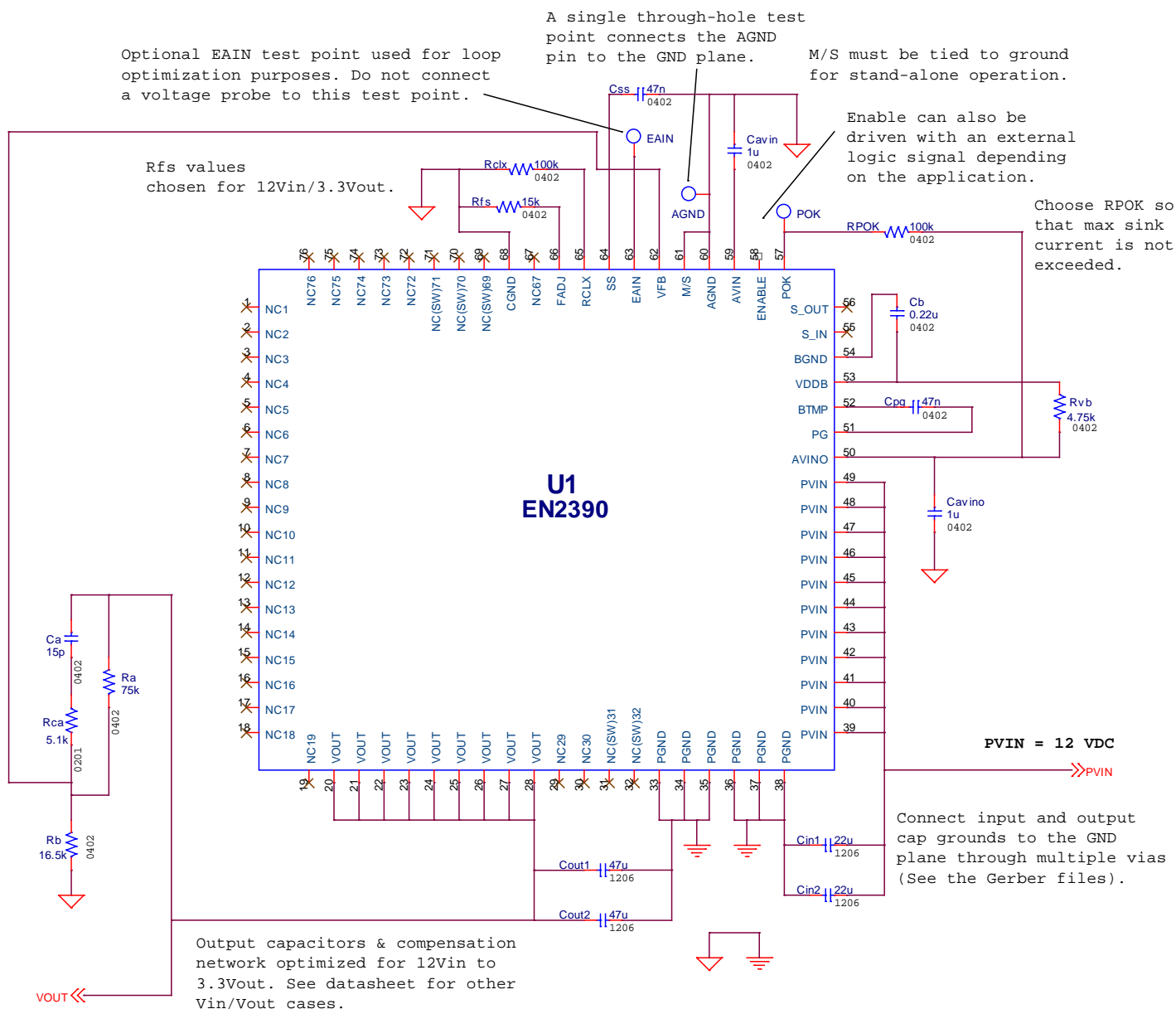


Figure 14: Engineering Schematic for Smallest Solution Size

Layout Recommendation

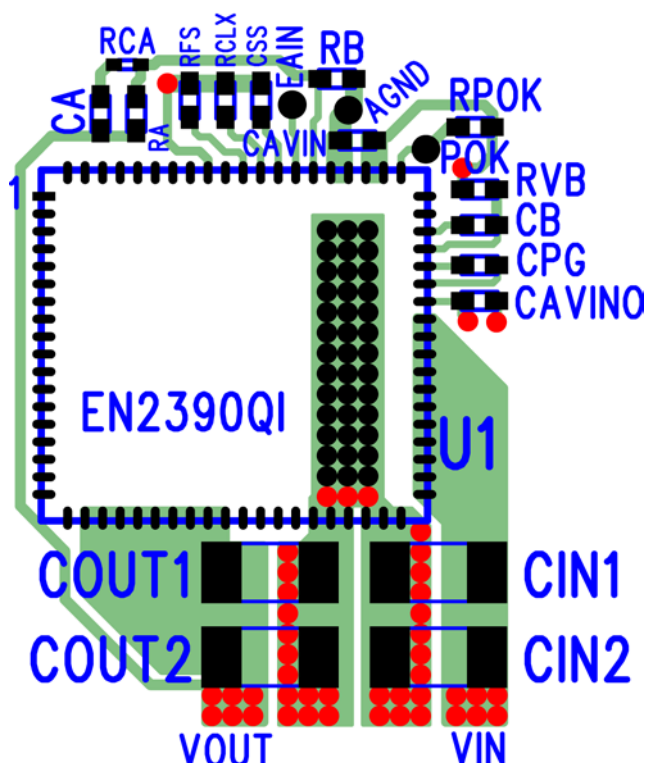


Figure 15: Critical Component Layout for Minimum Footprint (Top Layer). See Figure 14 for schematic.

This layout only shows the critical components and top layer traces for minimum footprint in single-supply, master mode with ENABLE tied to AVIN. Alternate circuit configurations & other low-power pins need to be connected and routed according to customer application. Please see the Gerber files at www.altera.com/enpirion for details on all layers.

Recommendation 1: Input and output filter capacitors should be placed on the same side of the PCB, and as close to the EN2390QI package as possible. They should be connected to the device with very short and wide traces. Do not use thermal reliefs or spokes when connecting the capacitor pads to the respective nodes. The +V and GND traces between the capacitors and the EN2390QI should be as close to each other as possible so that the gap between the two nodes is minimized, even under the capacitors.

Recommendation 2: The PGND connections for the input and output capacitors on layer 1 need to have a slit between them in order to provide some separation between input and output current loops.

Recommendation 3: The system ground plane should be the first layer immediately below the surface layer. This ground plane should be continuous and un-interrupted below the converter and the input/output capacitors.

Recommendation 4: The thermal pad underneath the component must be connected to the system ground plane through as many vias as possible. The drill diameter of the vias should be 0.33mm, and the vias must have at least 1 oz. copper plating on the inside wall, making the finished hole size around 0.20-0.26mm. Do not use thermal reliefs or spokes to connect the vias to the ground plane. This connection provides the path for heat dissipation from the converter.

Recommendation 5: Multiple small vias (the same size as the thermal vias discussed in recommendation 4) should be used to connect ground terminal of the input capacitor and output capacitors to the system ground plane. It is preferred to put these vias along the edge of the GND copper closest to the +V copper. These vias connect the input/output filter capacitors to the GND plane, and help reduce parasitic inductances in the input and output current loops. If vias cannot be placed under the capacitors, then place them on both sides of the slit in the top layer PGND copper.

Recommendation 6: AVIN is the power supply for the small-signal control circuits. It should be connected to the input voltage at a quiet point. In Figure 15 this connection is made at the input capacitor.

Recommendation 7: The layer 1 metal under the device must not be more than shown in Figure 13. Refer to the section regarding Exposed Metal on Bottom of Package. As with any switch-mode DC/DC converter, try not to run sensitive signal or control lines underneath the converter package on other layers.

Recommendation 8: The V_{OUT} sense point should be just after the last output filter capacitor. Keep the sense trace short in order to avoid noise coupling into the node. Contact Altera MySupport for any remote sensing applications.

Recommendation 9: Keep R_A , C_A , R_B , and R_{CA} close to the VFB pin (Refer to Figure 15). The VFB pin is a high-impedance, sensitive node. Keep the trace to this pin as short as possible. Whenever possible, connect R_B directly to the AGND instead of going through the GND plane.

Recommendation 10: Follow all the layout recommendations as close as possible to optimize performance. Altera provides schematic and layout reviews for all customer designs. Contact Altera MySupport for detailed support (www.altera.com/mysupport).

Design Considerations for Lead-Frame Based Modules

Exposed Metal on Bottom of Package

Lead-frames offer many advantages in thermal performance, in reduced electrical lead resistance, and in overall foot print. However, they do require some special considerations.

In the assembly process lead frame construction requires that, for mechanical support, some of the lead-frame cantilevers be exposed at the point where wire-bond or internal passives are attached. This results in several small pads being exposed on the bottom of the package as shown in Figure 16.

Only the thermal pad and the perimeter pads are to be mechanically or electrically connected to the PC board. The PCB top layer under the EN2390QI should be clear of any metal (copper pours, traces, or vias) except for the thermal pad. The “shaded-out” area in Figure 16 represents the area that should be clear of any metal on the top layer of the PCB. Any layer 1 metal under the shaded-out area runs the risk of undesirable shorted connections even if it is covered by soldermask.

The solder stencil aperture should be smaller than the PCB ground pad. This will prevent excess solder from causing bridging between adjacent pins or other exposed metal under the package. Please consult the EN2390QI QFN Package Soldering Guidelines for more details and recommendations.

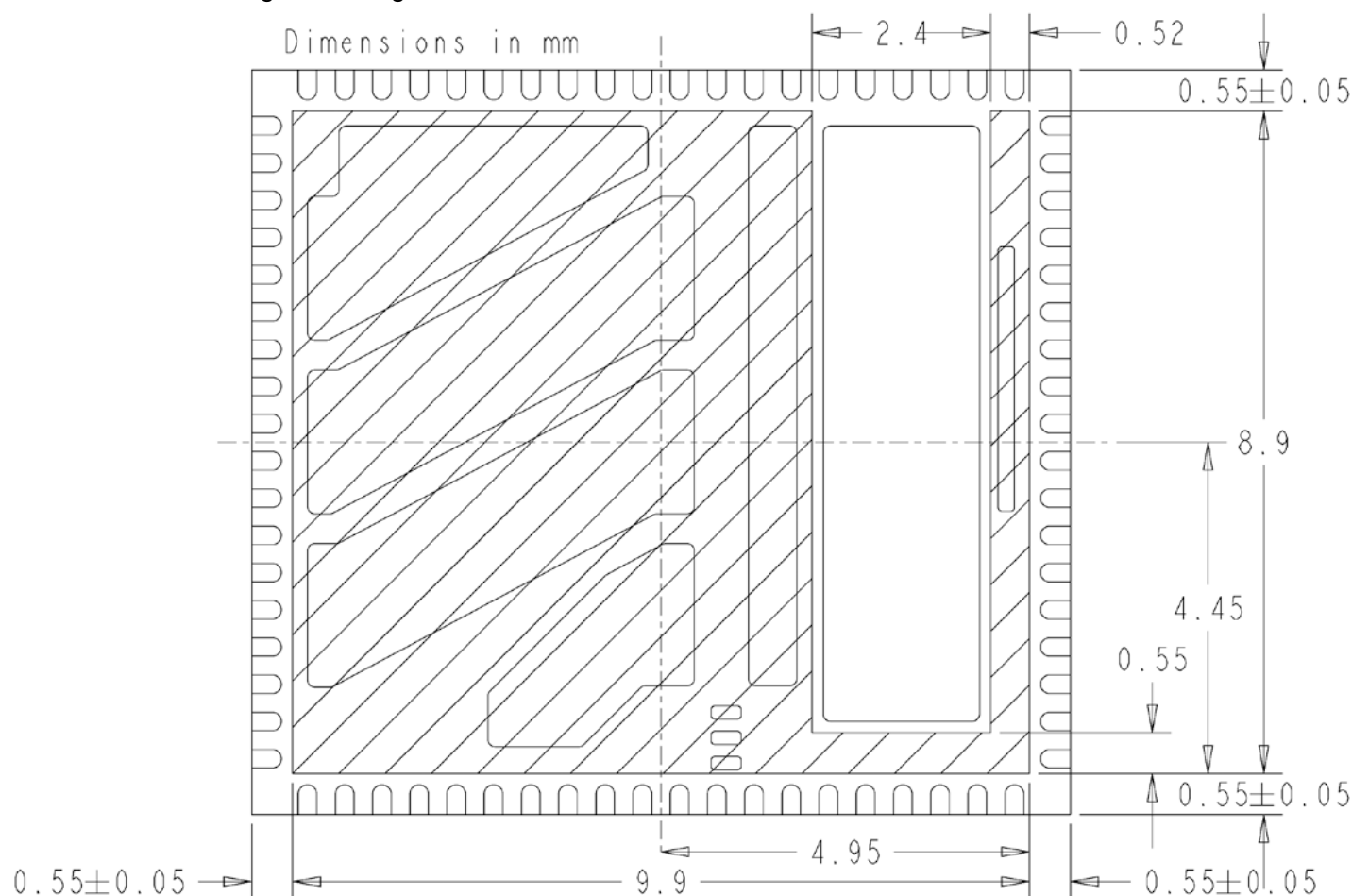


Figure 16: Lead-Frame exposed metal (Bottom View)

Shaded area highlights exposed metal that is not to be mechanically or electrically connected to the PCB.



The solder stencil aperture for the thermal pad (shown in blue) is based on Altera's manufacturing recommendations.



Packing and Marking Information: www.altera.com/support/reliability/packing/rel-packing-and-marking.html

Contact Information

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